

# Subducted material at the bottom of the mantle

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1. Original motivation: - PPV observed in the lower mantle in paleoslab areas  
- presumably weak

**What may be the dynamic consequences?**

2. Realistic model to study weak/strong PPV implications for slab dynamics

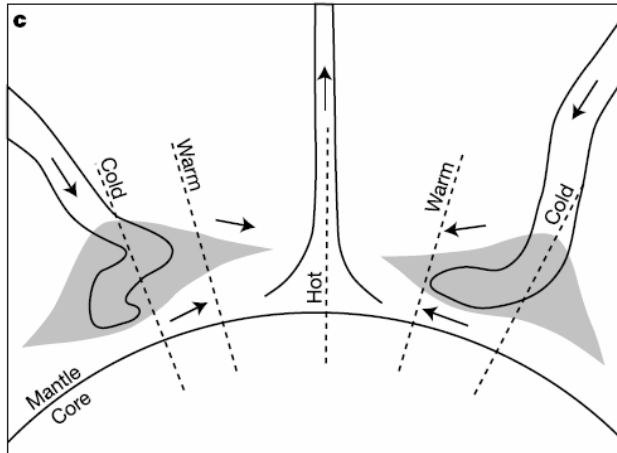
**BUT**

'realistic' expansivity does not allow for PPV formation

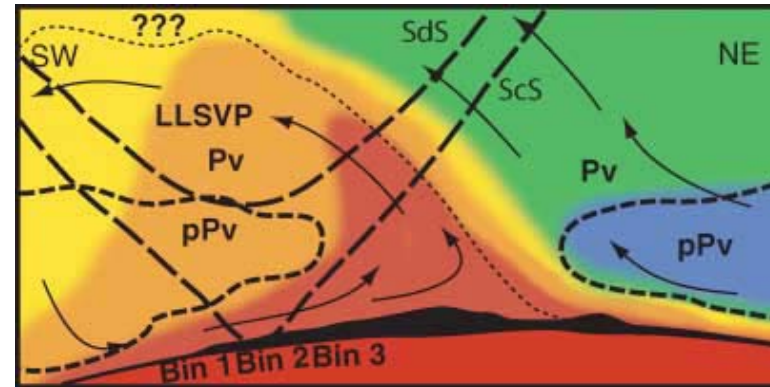


3. **Lower mantle slab deformation scenarios regardless PPV (comparison with subduction reconstructions)**

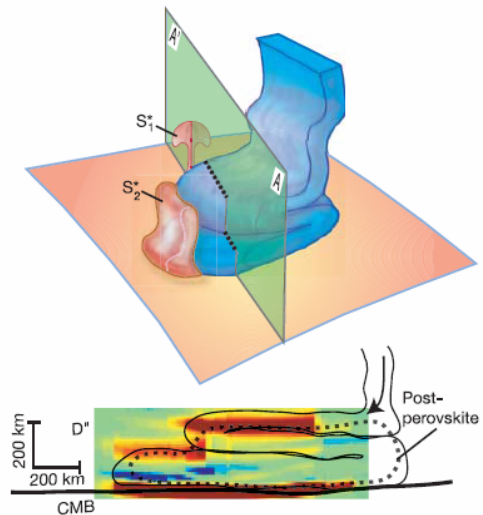
# PPV: OBSERVATIONS



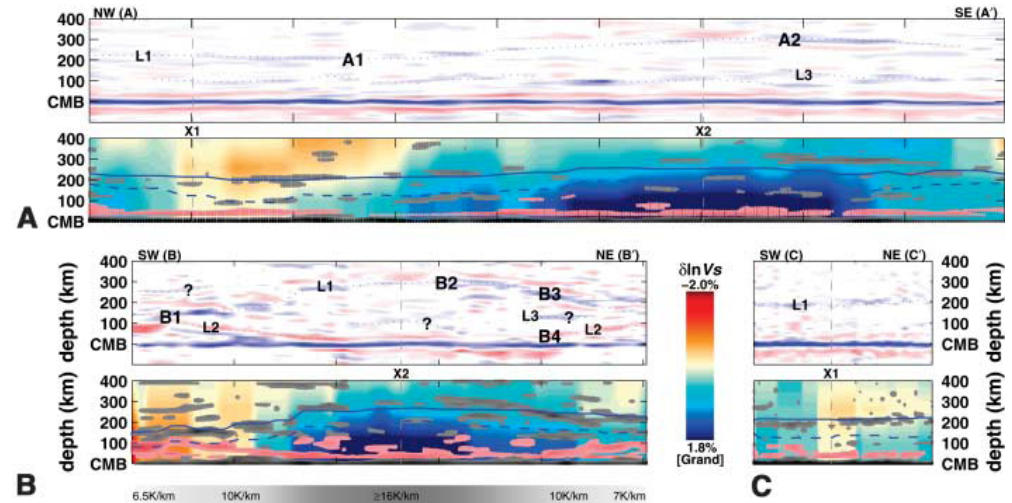
Hernlund et al., Nature 2005



Lay et al., Science 2006

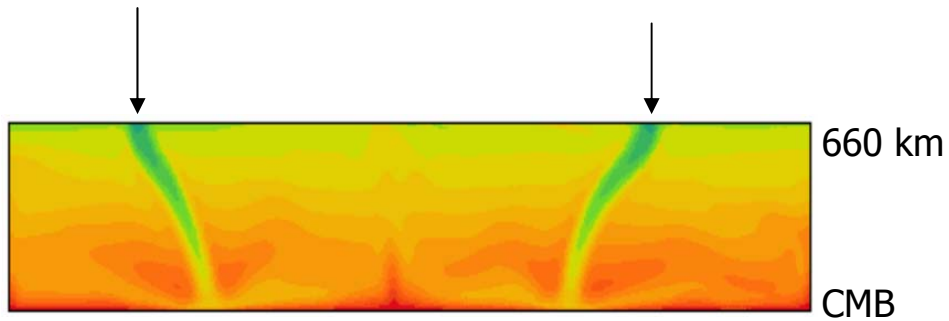


Hutko et al., Nature 2006

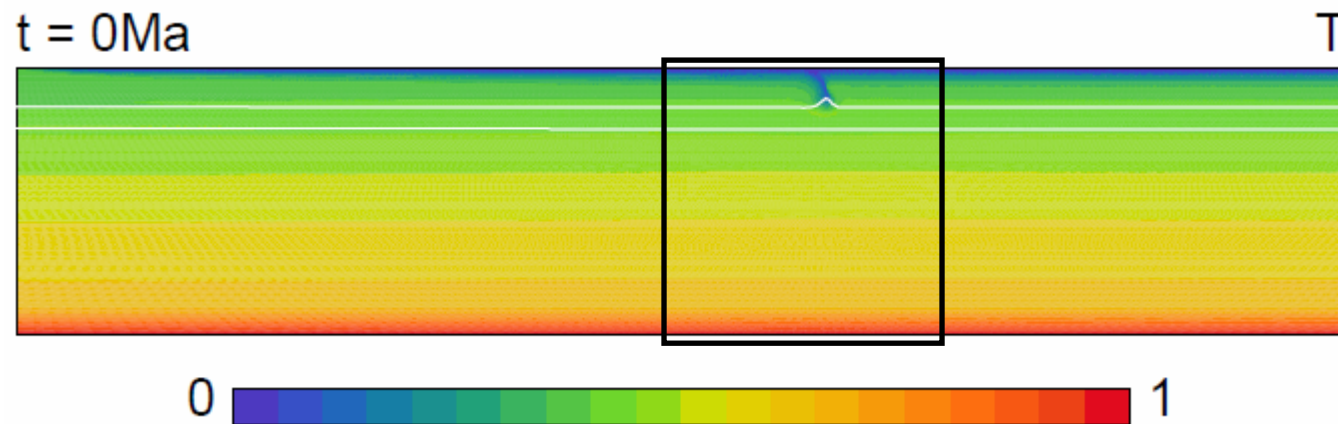


Van der Hilst et al., Science 2007

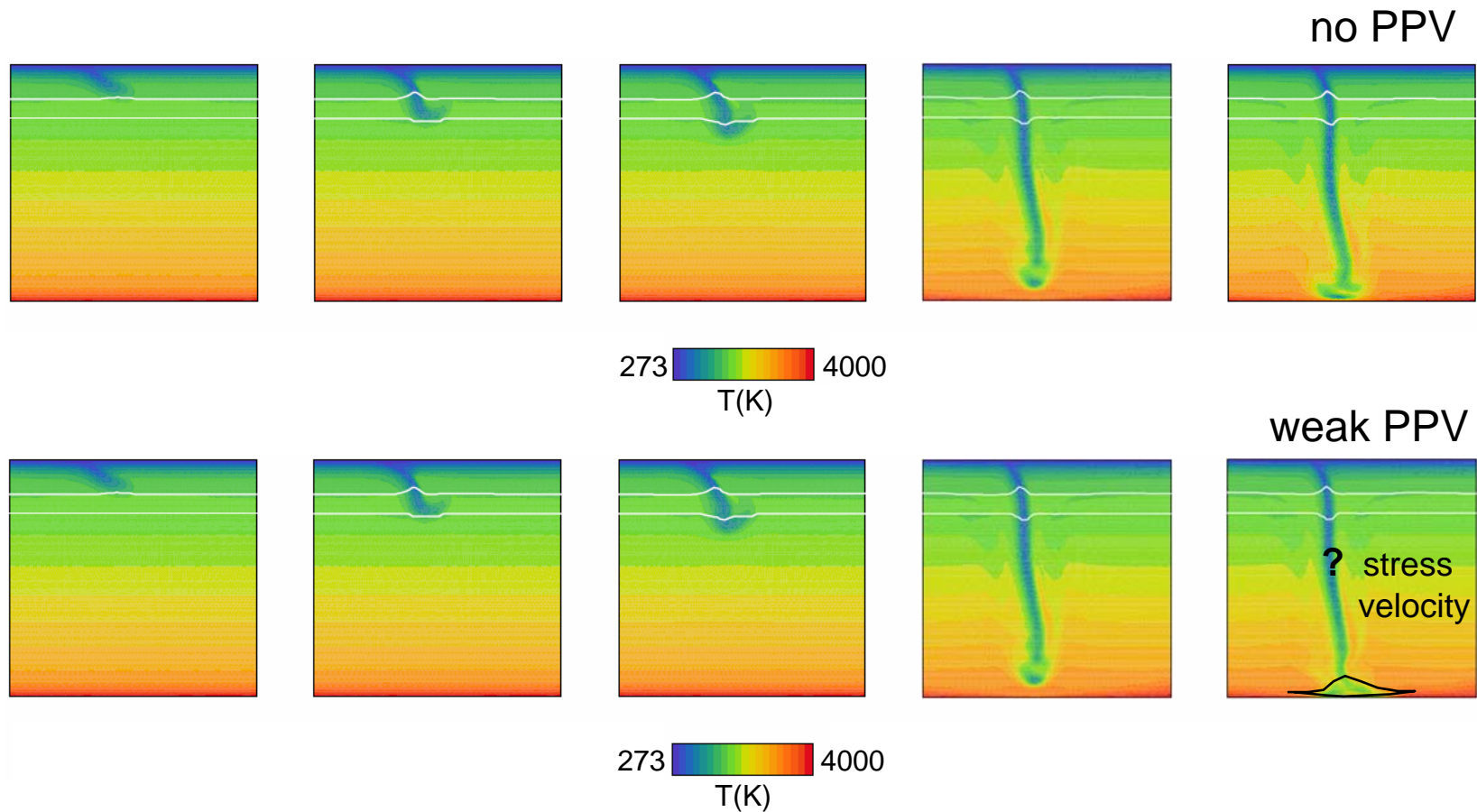
HOW DOES PPV RHEOLOGY INFLUENCE THE SLAB DEFORMATION AND  $D''$  DYNAMICS WITHIN THE COMPOSITE RHEOLOGICAL MODEL?



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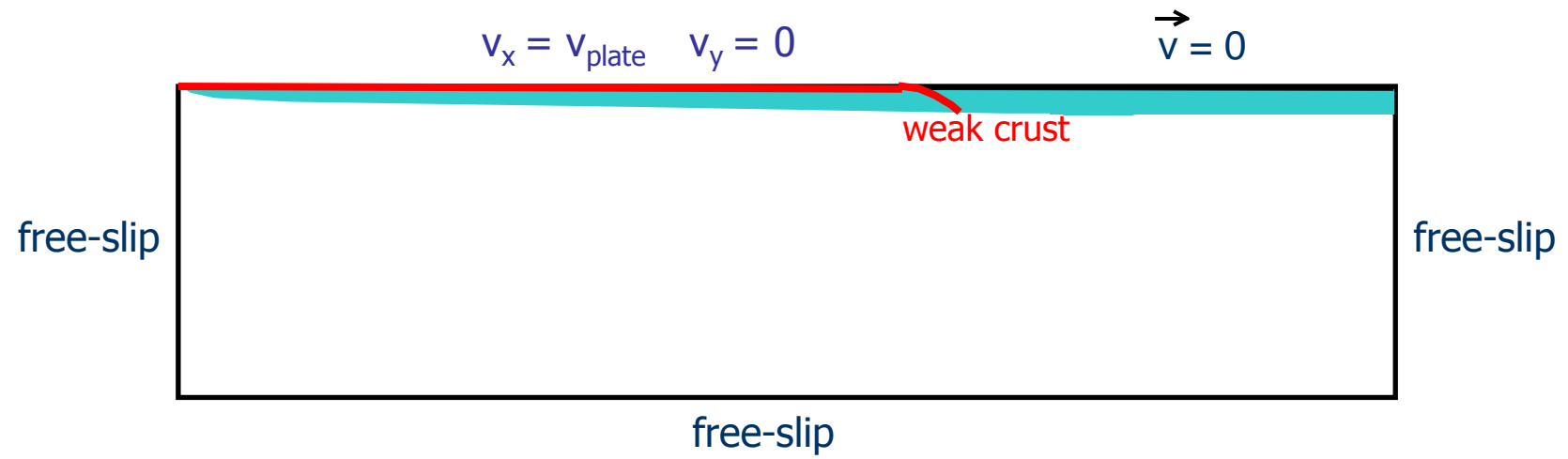


# HOW DOES PPV RHEOLOGY INFLUENCE THE SLAB DEFORMATION AND $D''$ DYNAMICS WITHIN THE COMPOSITE RHEOLOGICAL MODEL?

## MODEL

- 2D Cartesian box
- incompressible, extended Boussinesq
- viscous composite rheological model
- finite element code SEPRAN (Segal & Praagman, 2005)

# MODEL DOMAIN







# RHEOLOGY

viscous model:  $\dot{\varepsilon} = \dot{\varepsilon}_{diff} + \dot{\varepsilon}_{disl} + \dot{\varepsilon}_P$

diffusion creep  $\dot{\varepsilon}_{diff} = A_{diff} \sigma \exp\left(-\frac{E_{diff} + pV_{diff}}{RT}\right)$

dislocation creep  $\dot{\varepsilon}_{disl} = A_{disl} \sigma^n \exp\left(-\frac{E_{disl} + pV_{disl}}{RT}\right)$

Peierls creep  $\dot{\varepsilon}_P = A_P \exp\left[-\frac{H}{RT} \left(1 - \frac{\sigma}{\sigma_P}\right)^q\right]$

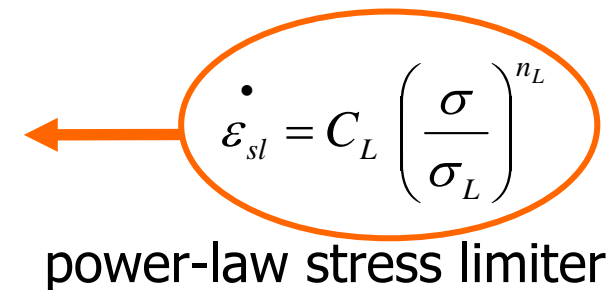
# RHEOLOGY

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$\dot{\varepsilon}_{sl} = C_L \left(\frac{\sigma}{\sigma_L}\right)^{n_L}$

power-law stress limiter

# RHEOLOGY

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power-law stress limiter  $\dot{\varepsilon}_{sl} = C_L \left(\frac{\sigma}{\sigma_L}\right)^{n_L}$  stress in the model can not exceed prescribed value of the yield stress ( $\sigma_L$ )

# CREEP PARAMETERS

$$A_{diff} = 1.0 \times 10^{-10} \text{ Pa}^{-1} \text{ s}^{-1}$$

$$E_{diff} = 3.35 \times 10^5 \text{ J mol}^{-1}$$

$$V_{diff} = 4.8 \times 10^{-6} \text{ m}^3 \text{ mol}^{-1}$$

$$A_{disl} = 1.13 \times 10^{-17} \text{ Pa}^{-1} \text{ s}^{-1}$$

$$E_{disl} = 4.8 \times 10^5 \text{ J mol}^{-1}$$

$$V_{disl} = 11 \times 10^{-6} \text{ m}^3 \text{ mol}^{-1}$$

## UPPER MANTLE

based on  
Hirth and Kohlstedt (2003)

$$A_{diff} = 9.25 \times 10^{-16} \text{ Pa}^{-1} \text{ s}^{-1}$$

$$E_{diff} = 2.0 \times 10^5 \text{ J mol}^{-1}$$

$$V_{diff} = 2.5 \times 10^{-6} \text{ m}^3 \text{ mol}^{-1}$$

## LOWER MANTLE

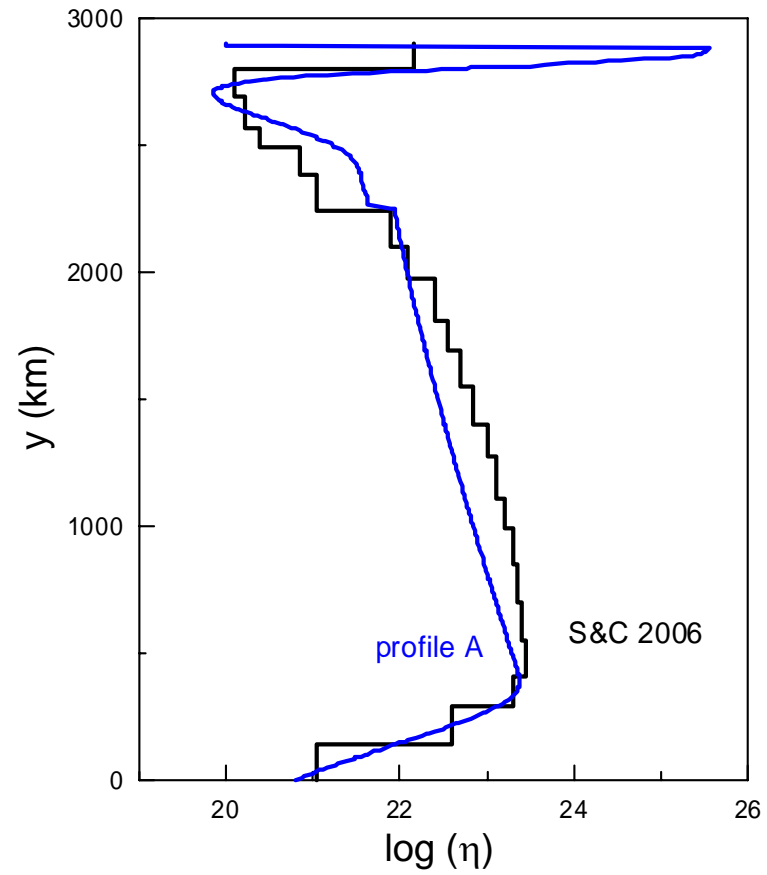
based on  
Yamazaki and Karato (2001)

+ power-law stress limiter with the yield stress  $\sigma_L = 10^8 \text{ Pa} - 10^9 \text{ Pa}$

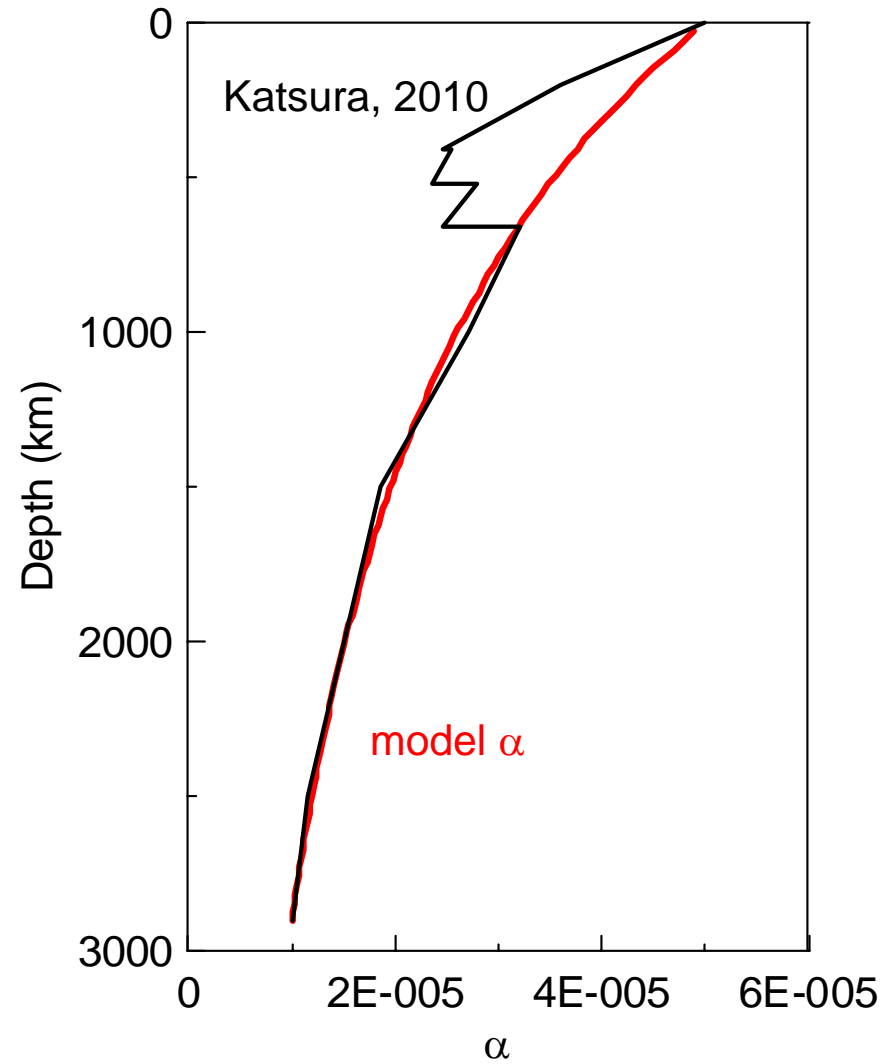
CRUST: constant viscosity  $\eta_C = 10^{20} \text{ Pas}$

PPV: constant viscosity  $\eta_{PPV} = 10^{20}, 10^{21} \text{ Pas}$

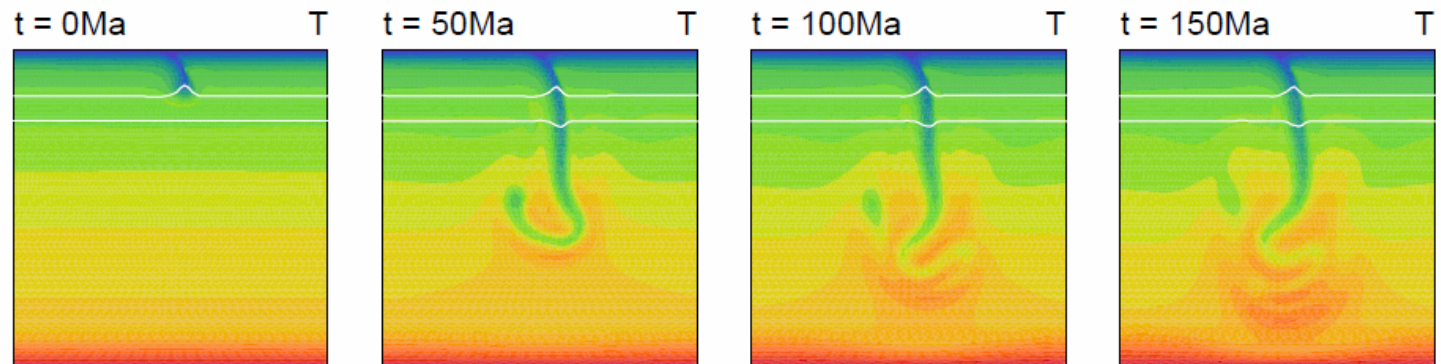
# VISCOSITY PROFILE



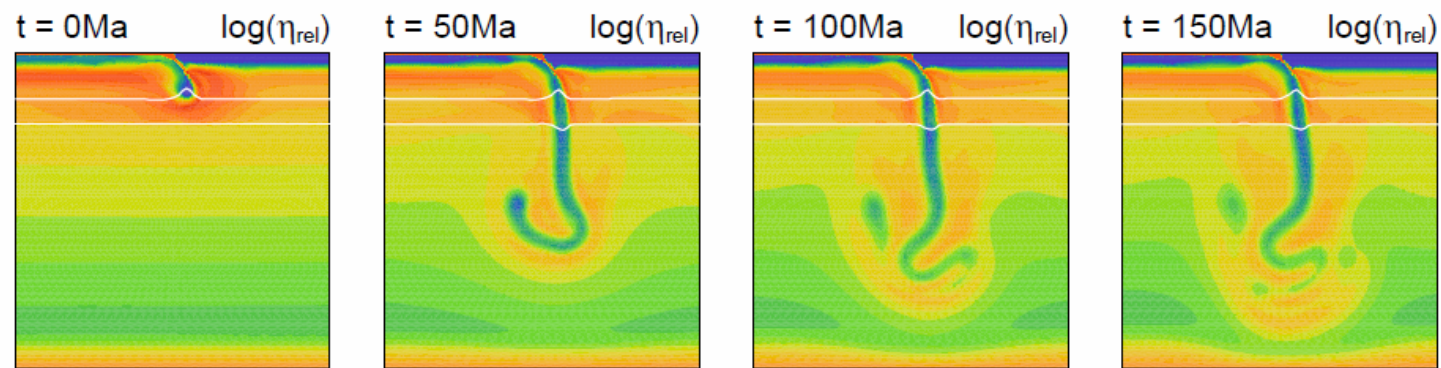
# EXPANSIVITY PROFILE




# VISCOSITY PROFILE A: TIME EVOLUTION



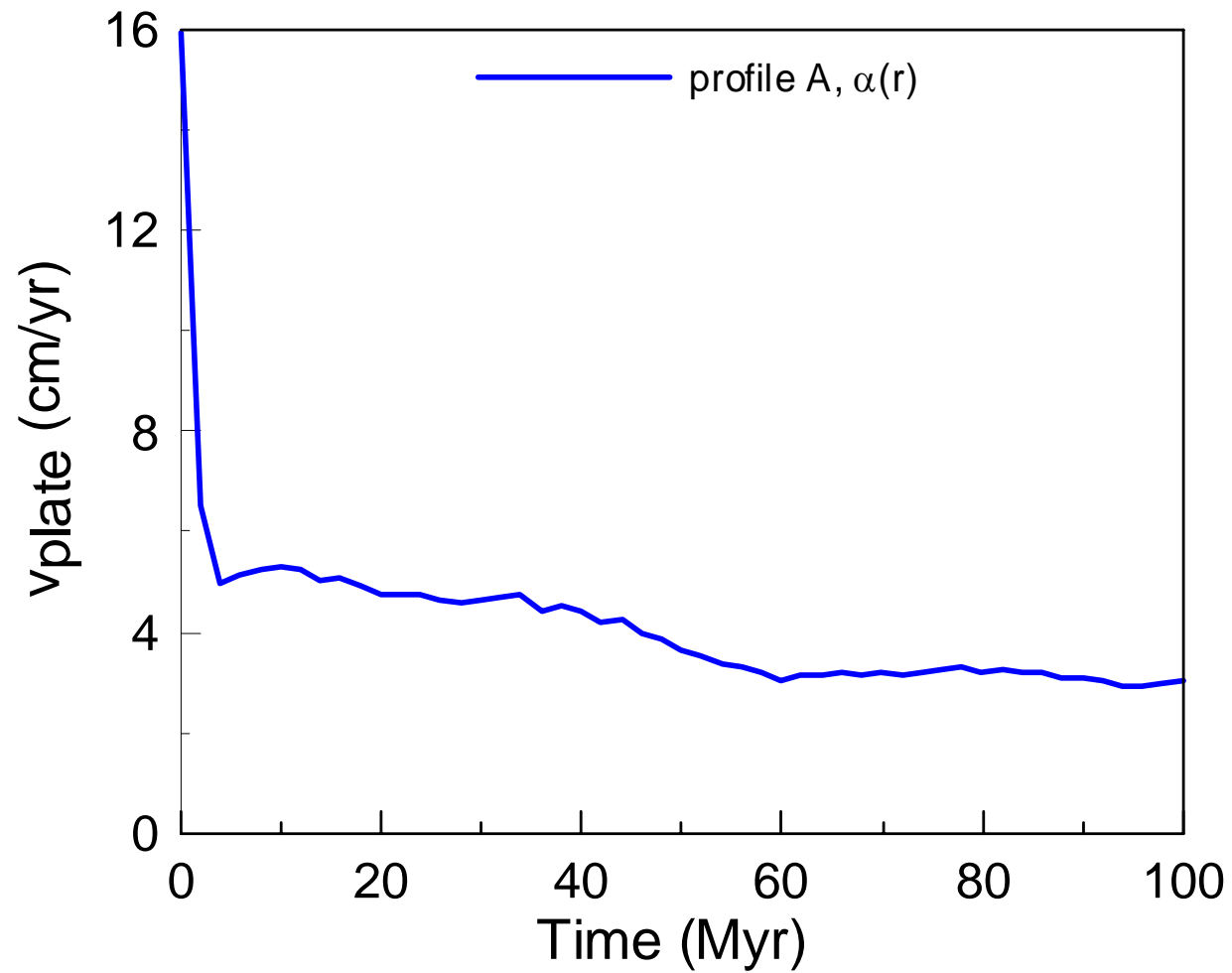
273  4000 K



-2  5  
 $\log(\eta_{\text{rel}})$



# VISCOSITY PROFILE A: PLATE VELOCITY



Slab in the lower mantle is too warm to transform to PPV

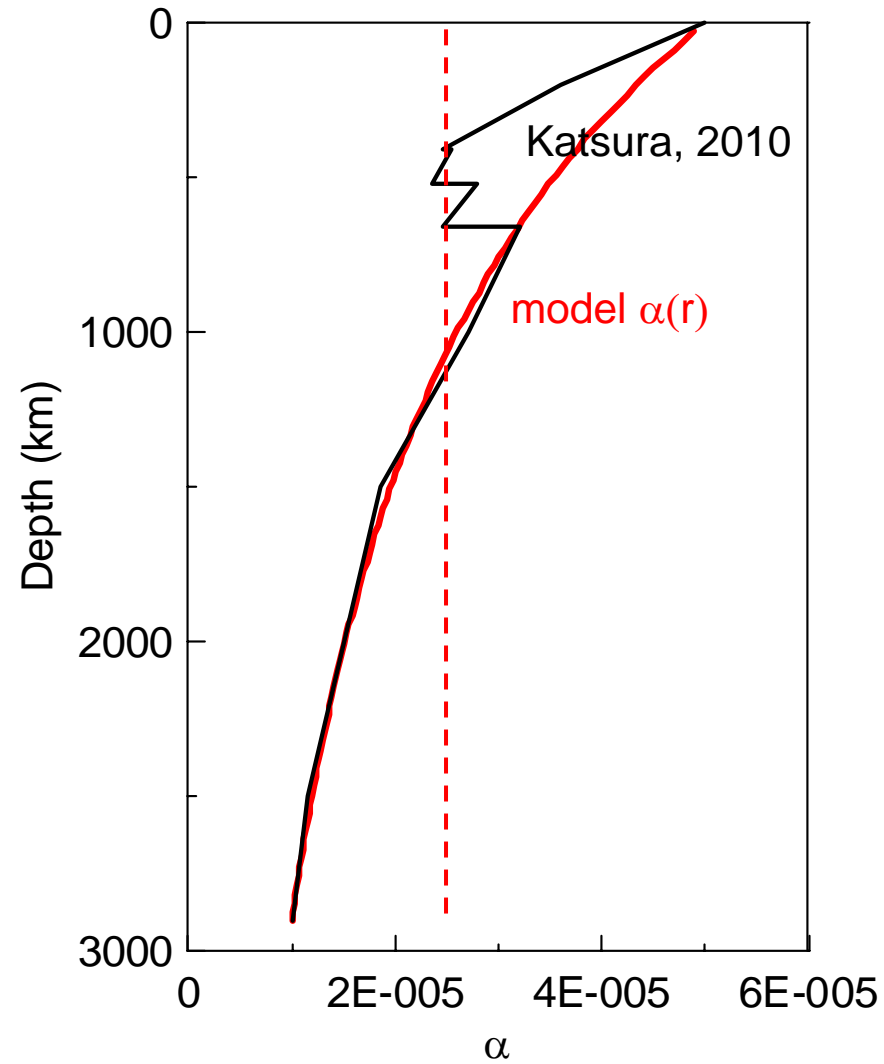
**How we could reach the PPV stability conditions?**

We need colder slab arriving to the CMB

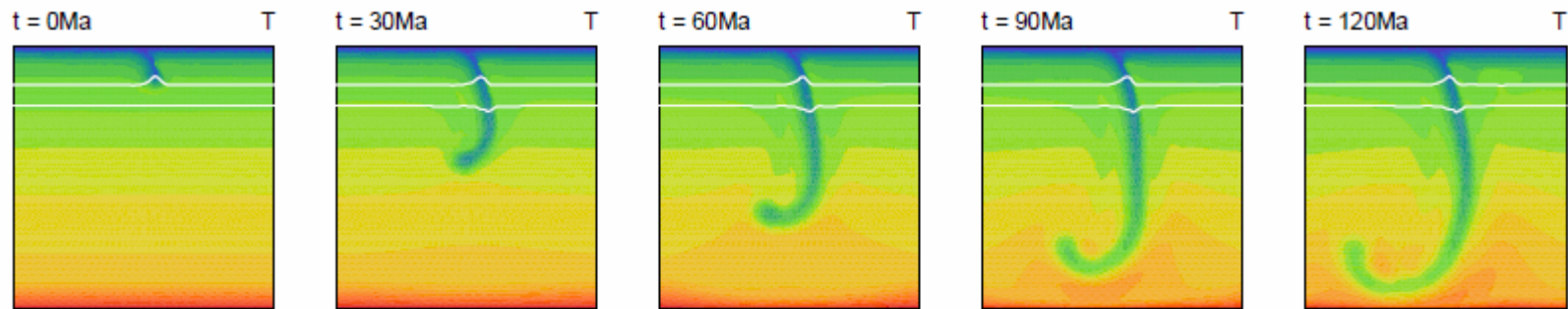
– we need to get rid of the viscous heating due to the slab slowing down

Constant expansivity?

# EXPANSIVITY PROFILE 2

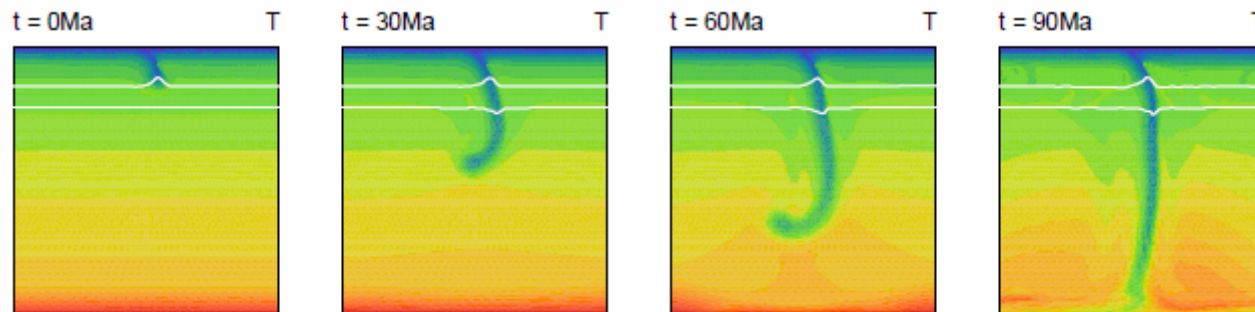


# VISCOSITY PROFILE A + CONSTANT $\alpha$ : TIME EVOLUTION



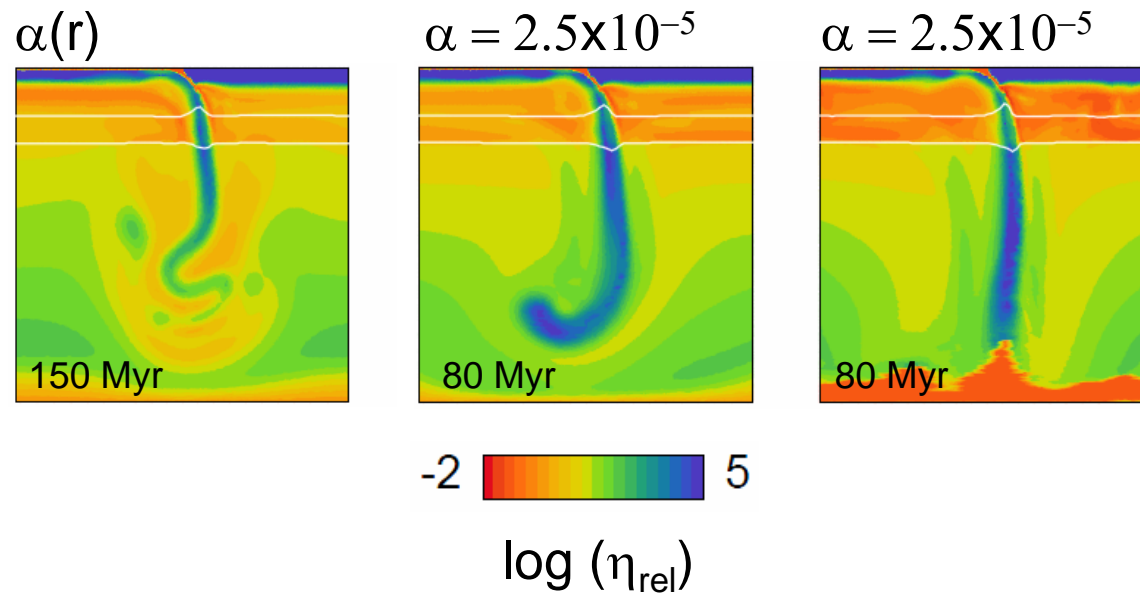
273  4000 K

+ WEAK PPV ( $\eta = 10^{20}$  Pas)

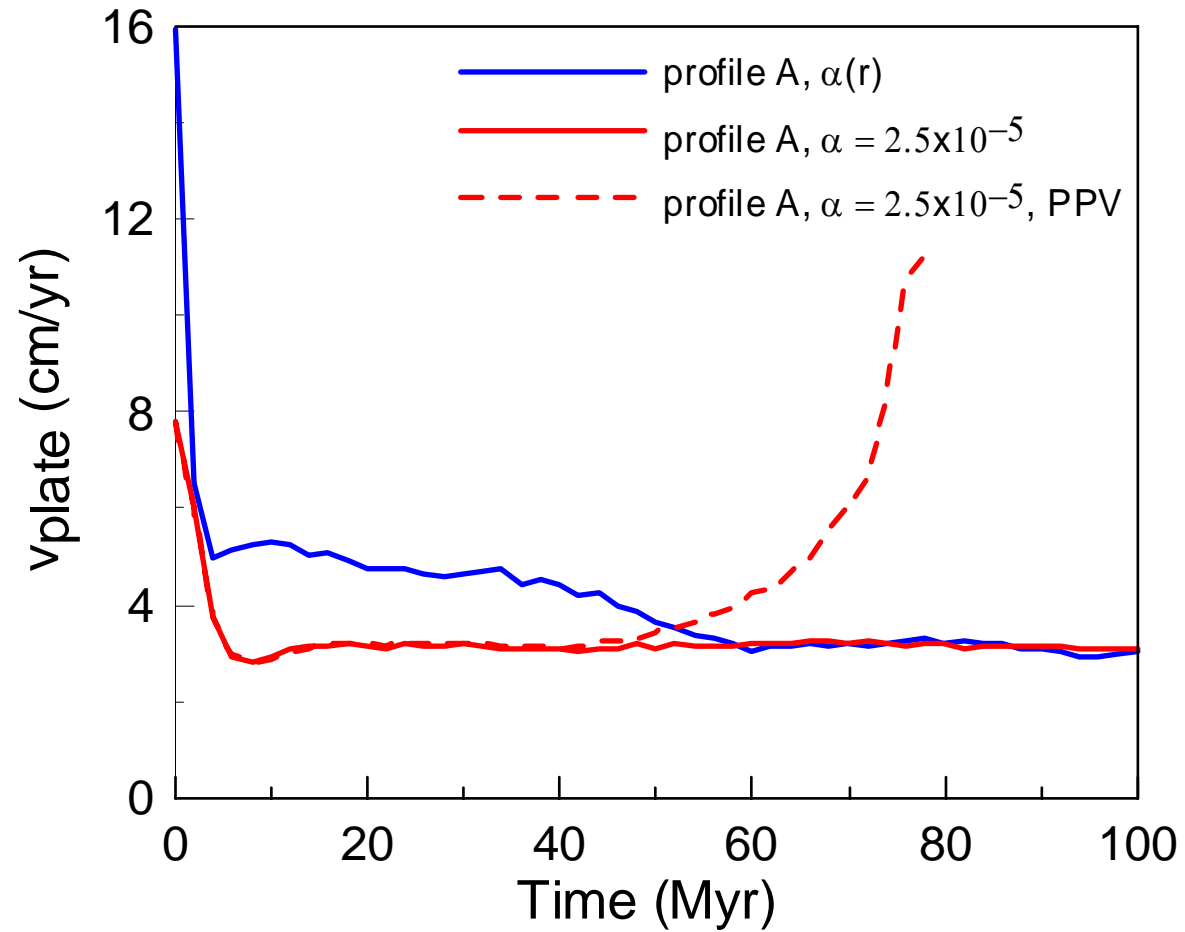


273  4000 K

# VISCOSITY PROFILE A



# VISCOSITY PROFILE A: PLATE VELOCITY



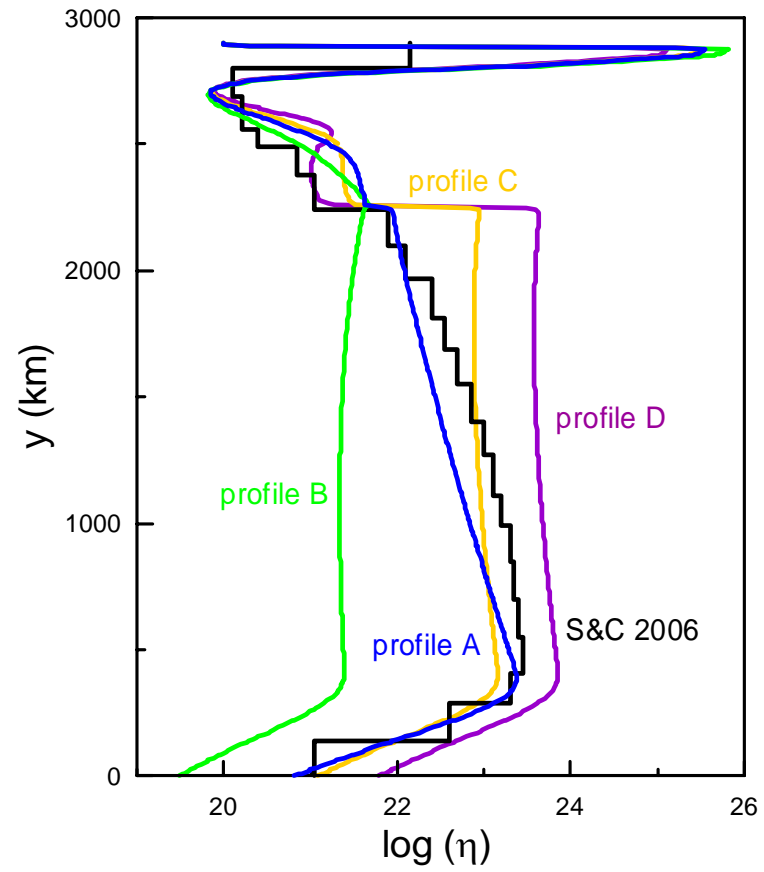
Constant expansivity allows for PPV formation

**BUT**

expansivity **should** be decreasing

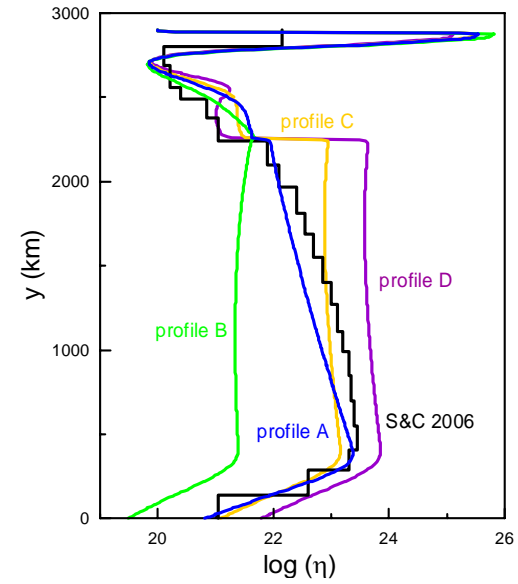
Could other viscosity profile help?

# VISCOSITY PROFILES

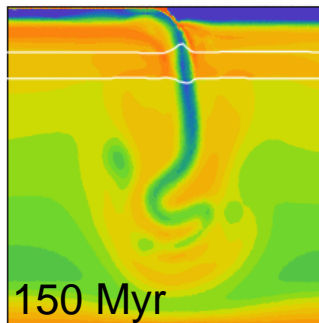




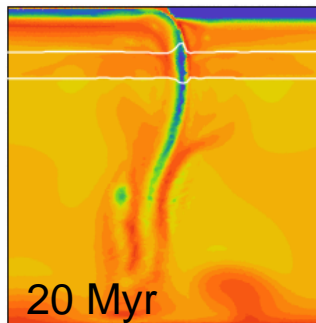
# DECREASING EXPANSIVITY $\alpha(r)$ : EFFECT OF VISCOSITY PROFILE



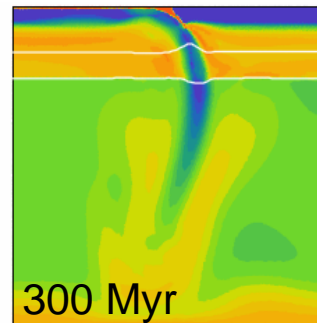
A  $\alpha(r)$



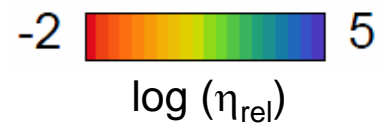
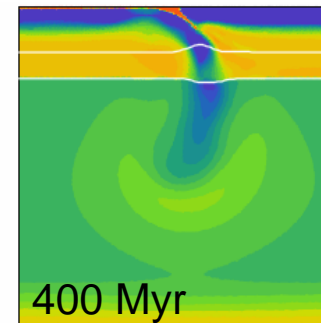
B  $\alpha(r)$



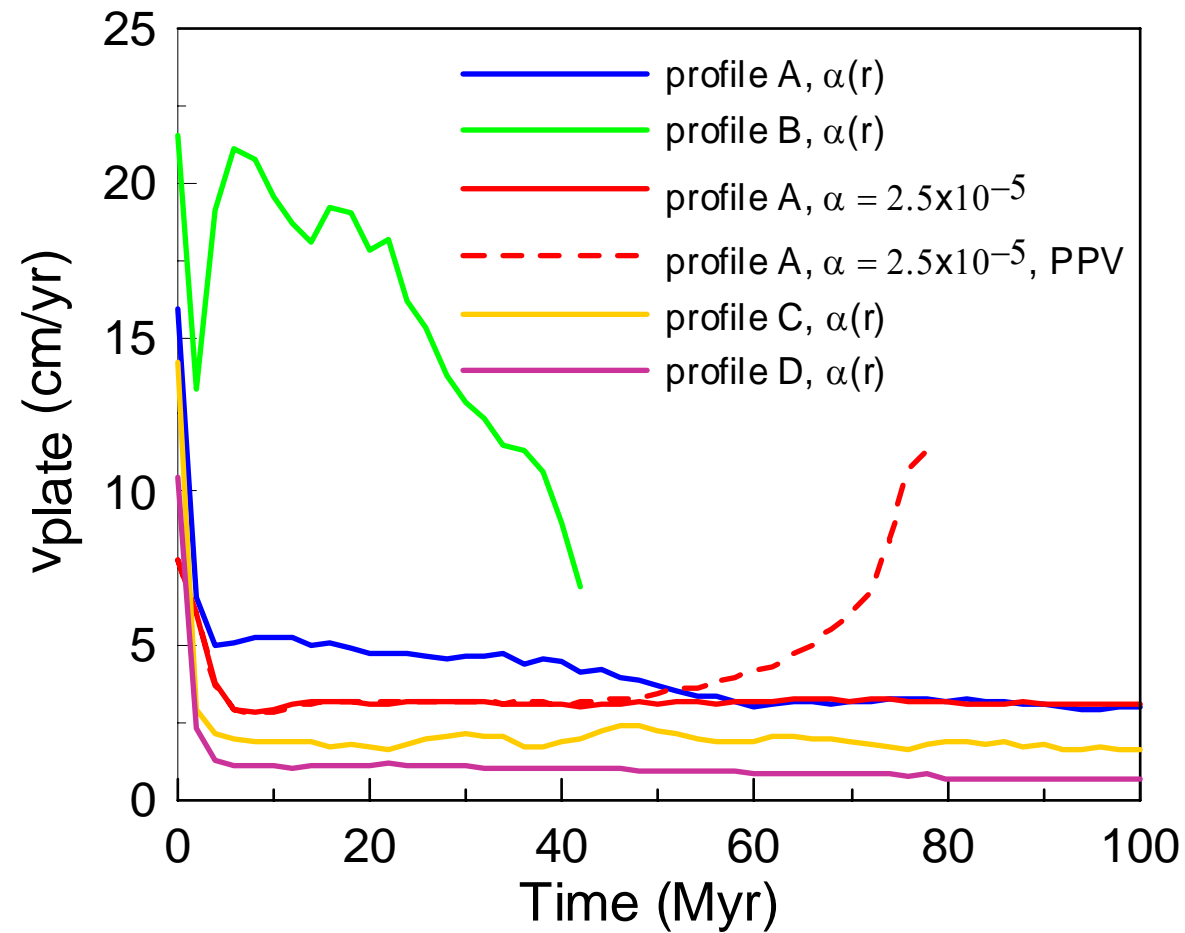
C  $\alpha(r)$



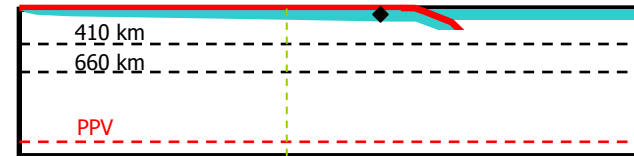
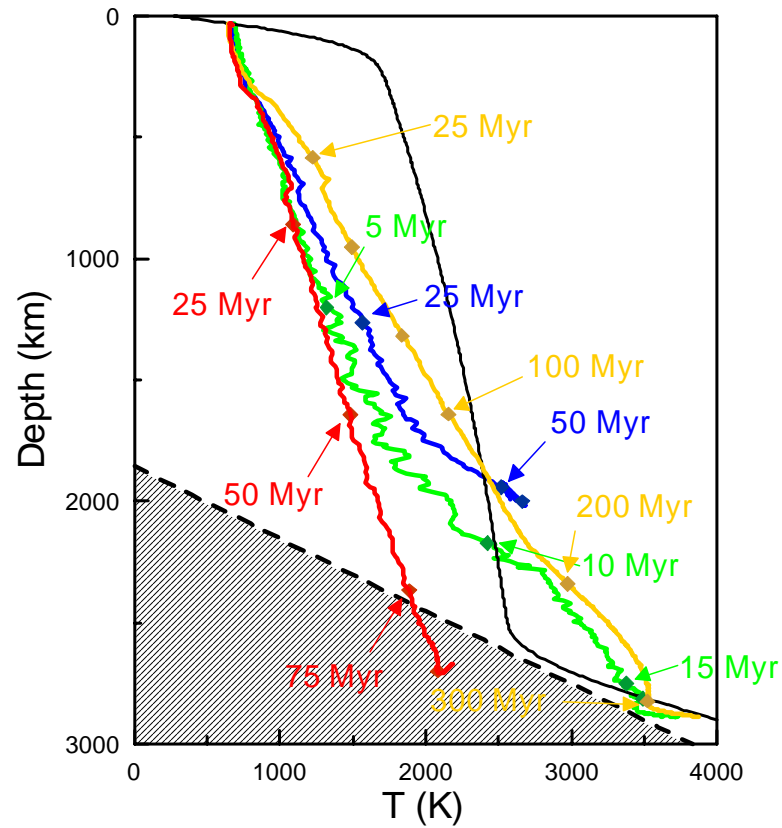
D  $\alpha(r)$



# VISCOSITY PROFILES A-D: PLATE VELOCITY



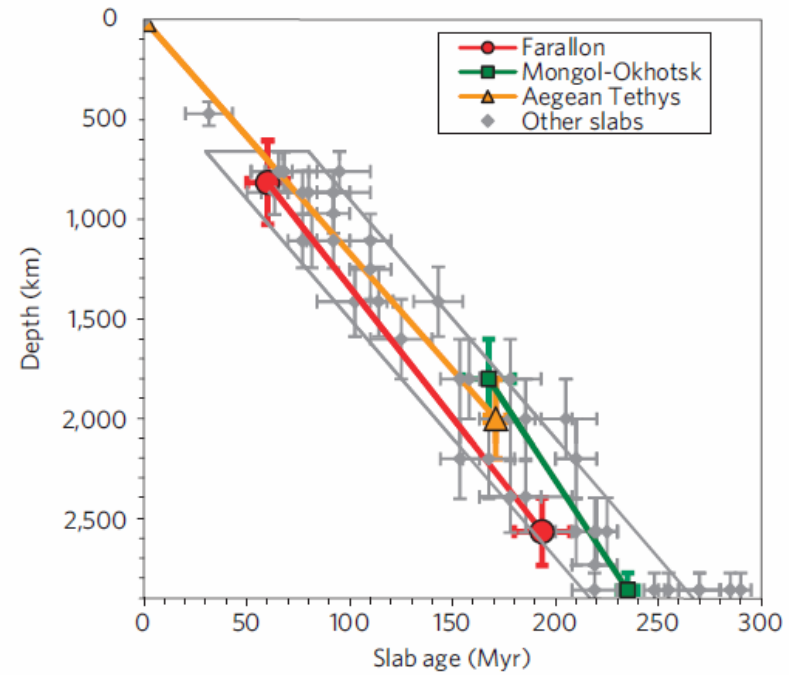
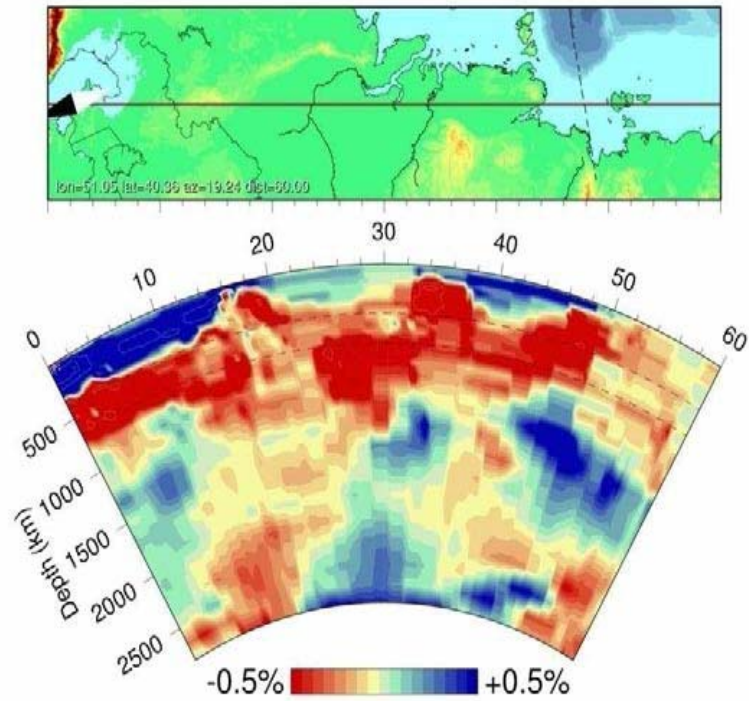
# TEMPERATURE OF THE MONITOR TRACER



Tracer temperature (K)

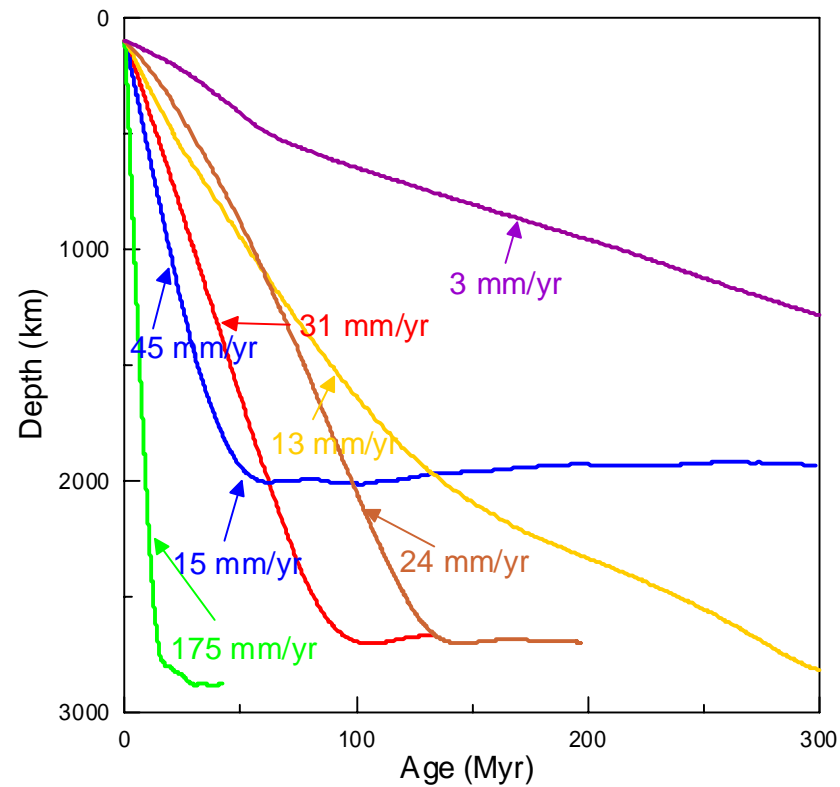
- viscosity A,  $\alpha = 2.5 \times 10^{-5}$
- viscosity A,  $\alpha(r)$
- viscosity B,  $\alpha(r)$
- viscosity C,  $\alpha(r)$
- initial geotherm

# VAN DER MEER ET AL. (2010)



SINKING VELOCITY ~ 12 mm/yr

# DEPTH vs. AGE: SINKING VELOCITIES



- profile A,  $\alpha=2.5 \times 10^{-5}$
- profile A,  $\alpha(r)$
- profile B,  $\alpha(r)$
- profile C,  $\alpha(r)$
- profile C,  $\alpha=2.5 \times 10^{-5}$
- profile D,  $\alpha(r)$

Viscosity profile C produces sinking velocity of about  
1 cm/yr

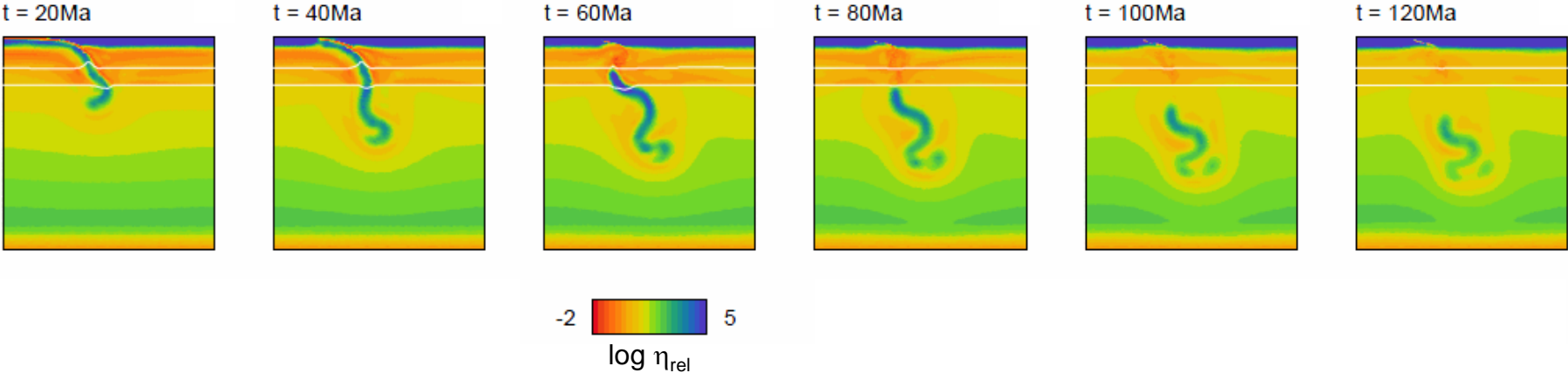
**BUT**

Van der Meer et al. (2010) derived it for the **detached** slab

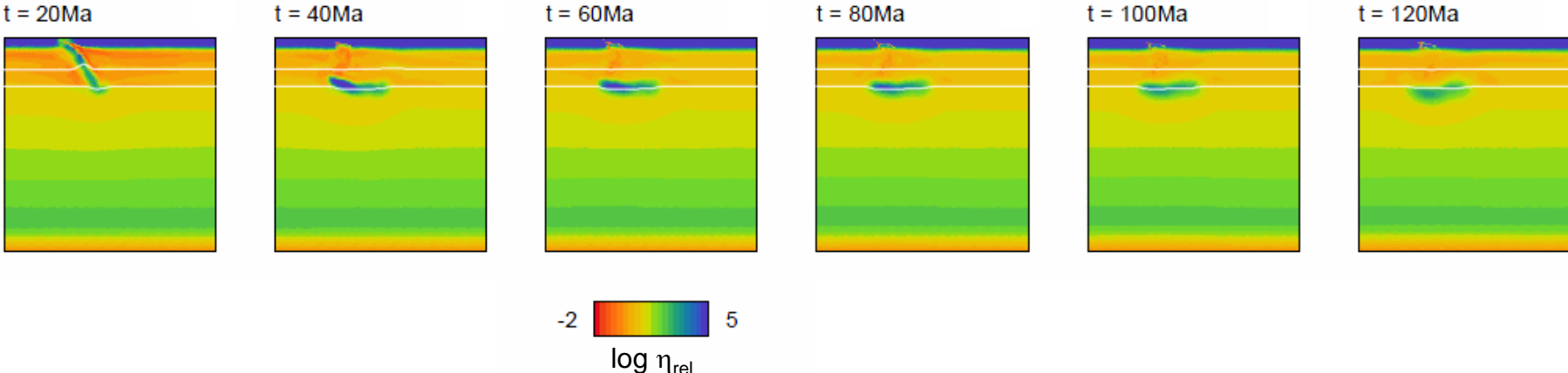
What would be the sinking velocities of the detached slabs?

# SLAB BREAK-OFF: VISCOSITY PROFILE A

## CRUSTAL SEGMENT 2000 KM

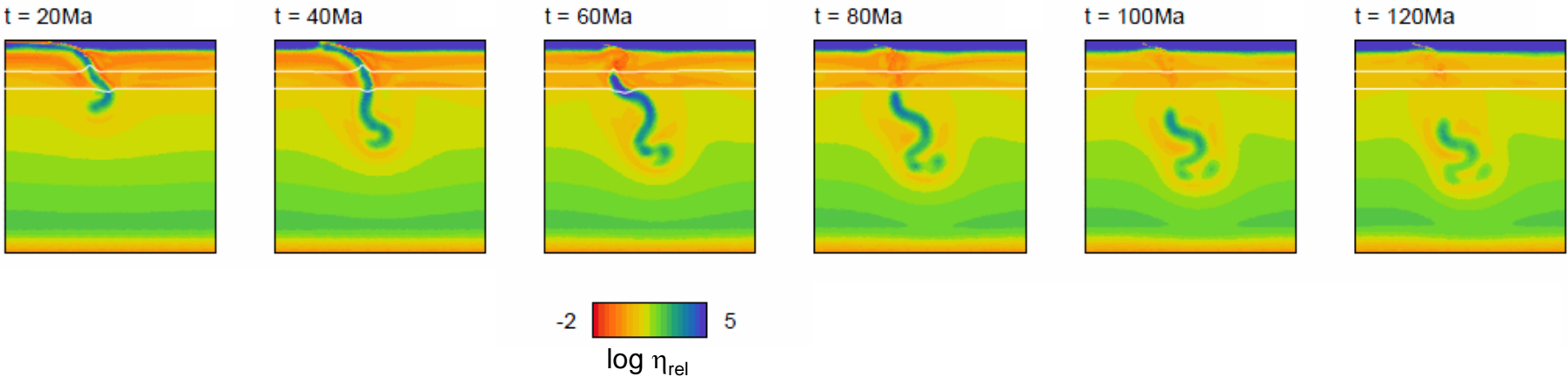


## CRUSTAL SEGMENT 500 KM

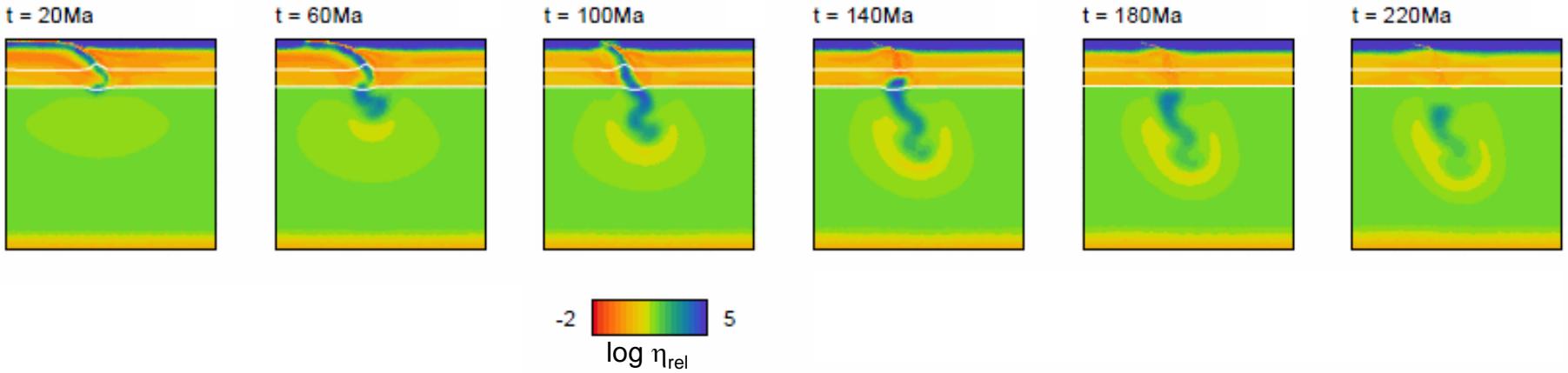


# SLAB BREAK-OFF: CRUSTAL SEGMENT 2000 km

## VISCOSITY PROFILE A

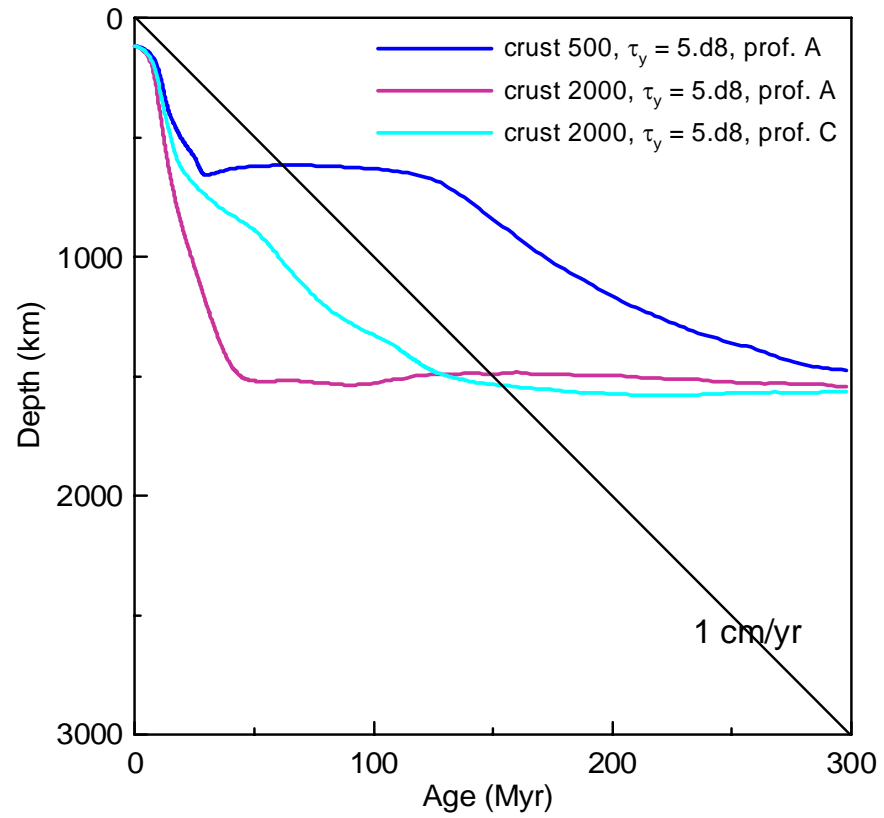


## VISCOSITY PROFILE C



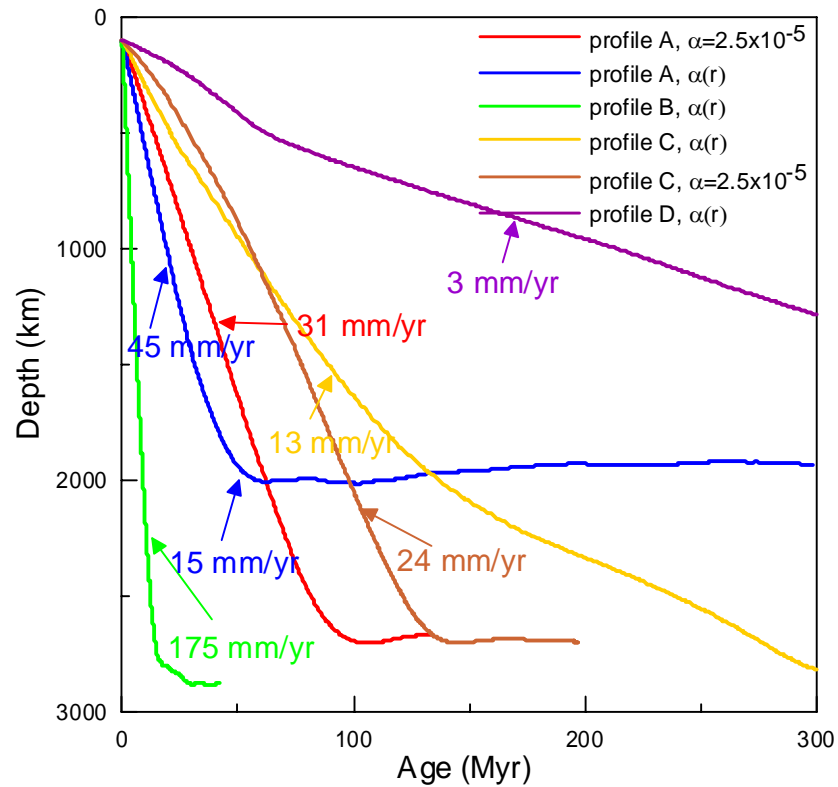


# DEPTH vs. AGE: SINKING VELOCITIES

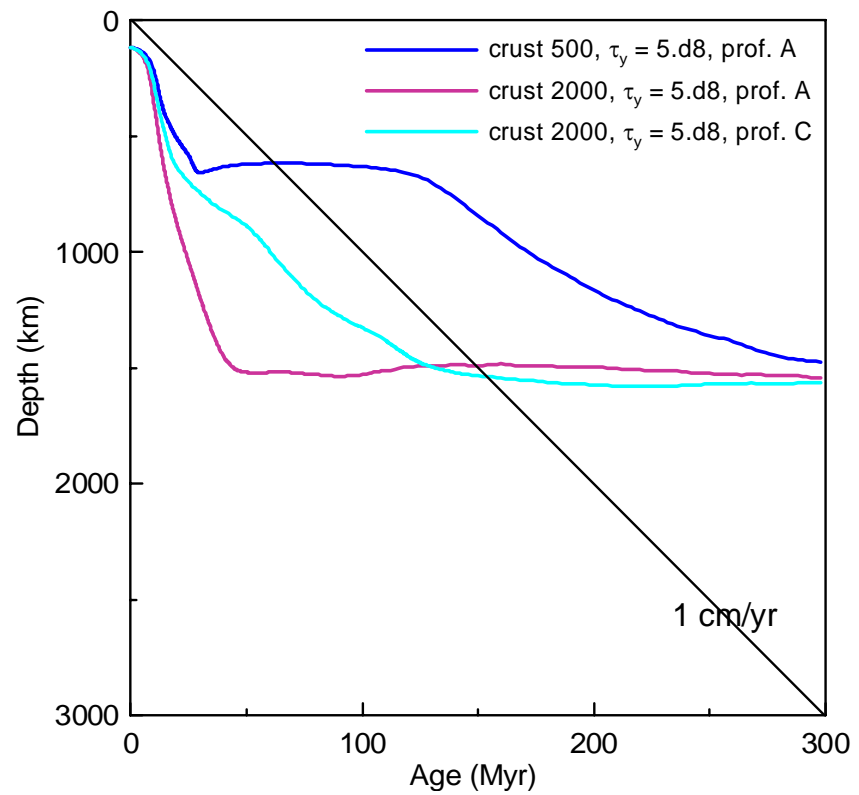


# DEPTH vs. AGE: SINKING VELOCITIES

## CONTINUOUS SLAB



## DETACHED SLAB



## CONCLUSIONS

The dynamics of the subducted slab in the lower mantle is very sensitive to the depth dependent expansivity and rheology

If the expansivity follows the curve by Katsura (2010), cold slab does not reach the base of the mantle and no PPV is formed

Slab sinking velocities are in agreement with the reconstructions by Van der Meer et al. (2010) for the lower mantle viscosity of about  $10^{23}$  Pas

Detached slabs never reach the bottom of the mantle

Sinking velocities for the detached slab may differ from those for the continuous slab



More detailed study of the combined effects of the lower mantle viscosity and expansivity will be necessary to obtain a reasonable fit to the slab reconstructions